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جزوه درس:

مقاومت مصالح 2

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با استفاده از جزوات اسکن شده، به محیط زیست کمک کنیم...

هر آنچه که در این جزوه می خوانید حاصل زحمات دانشجویان دانشگاه صنعتی شریف می باشد که دانسته های خود از حضور در کلاس استاد محترم، دکتر عاصم پور را مکتوب کرده اند.

استفاده از این جزوات برای تمامی دانشجویان کاملا رایگان می باشد.

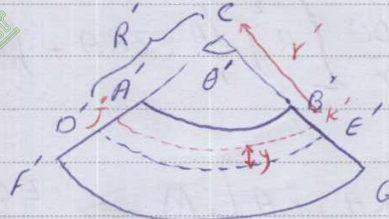
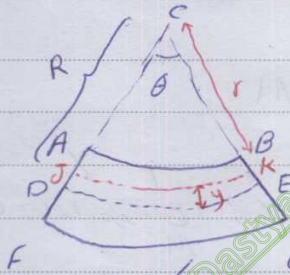


Subject: *مکانیک جامدات*

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تغییرات هندسی

فرض برهما صبره



سطح مقطع قبل از تغییرات هندسی

$R\theta = R'\theta'$

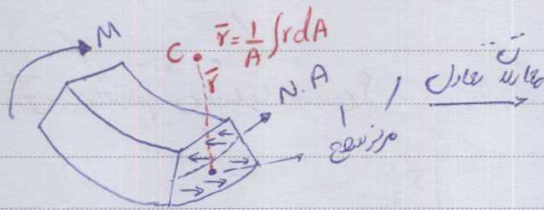
تغییرات هندسی: $R \rightarrow R'$ و $\theta \rightarrow \theta'$

$$\left. \begin{aligned} JK &= r\theta \\ J'K' &= r'\theta' \end{aligned} \right\} \rightarrow \delta = r'\theta' - r\theta$$

$$\left. \begin{aligned} r &= R - y & \delta &= (R' - y)\theta' - (R - y)\theta \\ r' &= R' - y & \theta' - \theta &= \Delta\theta \\ \theta' - \theta &= \Delta\theta & \delta &= -y\Delta\theta \end{aligned} \right\}$$

بسی $\rightarrow \epsilon_x = \frac{\delta}{r\theta} = \frac{y\Delta\theta}{r\theta}$

$$\epsilon_x = -\frac{\Delta\theta}{\theta} \frac{y}{R-y} \quad \sigma_x = E\epsilon_x$$



$$\sum \sigma_x dA = 0$$

$$\sum y \sigma_x dA = M$$

$$\int \sigma_x dA \stackrel{①}{=} -\int \frac{E\Delta\theta}{\theta} \frac{R-y}{r} dA = 0 \Rightarrow \int \frac{R-y}{r} dA = 0$$

$$\rightarrow R \int \frac{dA}{r} - \int dA = 0 \rightarrow R = \frac{A}{\int \frac{dA}{r}} \quad ②$$

$$\int y \sigma_x dA = M \rightarrow \int \frac{E\Delta\theta}{\theta} \frac{R-y}{r} y dA = M \rightarrow \frac{E\Delta\theta}{\theta} \int \frac{(R-y)^2}{r} dA = M$$



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$$\bar{r} = \frac{1}{A} \int r dA \quad \left\{ \begin{array}{l} \frac{E \Delta \theta}{\theta} \left[R \int \frac{dA}{r} - 2RA + \int r dA \right] = M \\ e = \bar{r} - R \end{array} \right.$$

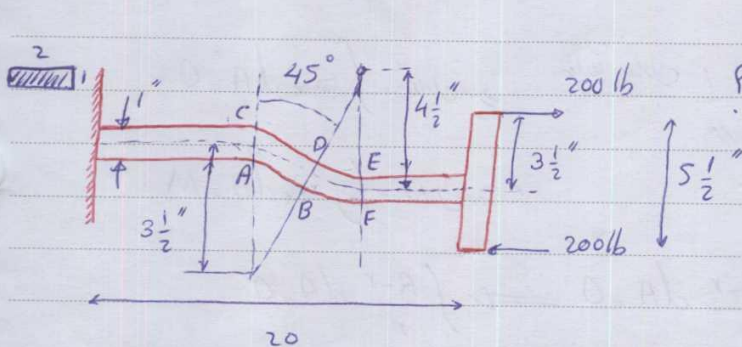
$$\rightarrow \frac{E \Delta \theta}{\theta} [RA - 2RA + \bar{r}A] = M \Rightarrow \frac{E \Delta \theta}{\theta} = \frac{M}{(\bar{r} - R)A} = \frac{M}{eA}$$

$$\rightarrow \sigma_x = - \frac{M y}{Ae(R-y)} = - \frac{M(r-R)}{Aer}$$

$$R\theta = R'\theta' \rightarrow \frac{1}{R'} = \frac{1}{R} \frac{\theta'}{\theta} = \frac{1}{R} \left(1 + \frac{\Delta \theta}{\theta}\right) = \frac{1}{R} \left(1 + \frac{M}{EAe}\right)$$

$$\rightarrow \frac{1}{R'} - \frac{1}{R} = \frac{M}{EAeR}$$

فوب است وقت e تا چار هم است، اینست



سؤال: ما کوروس هم است، اینست؟

$$M = 200 \times \left(5 \frac{1}{2}\right) = 1100 \text{ lb. in } \curvearrowright \quad \sigma = \frac{M y}{Ae(R-y)} \quad \left| \begin{array}{l} R = \frac{A}{s} = \frac{h}{\ln \frac{r_2}{r_1}} \\ \text{CD رادیوس } R = \frac{1}{3} = 3.485 \end{array} \right.$$

$$e = \bar{r} - R = 3.5 - 3.485 = 0.015''$$

$$\sigma = \frac{1100 \times (0.485)}{(2)(0.015)(14)} = 4720 \text{ psi}$$

در 4/3 سطح است، CD رادیوس

تشریح است در CD



4.173, 4.160

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79 -7
75 -7

$$\sigma_x = \frac{1100 \times (0.515)}{(2)(0.015)(3)} = 5930 \text{ psi} \quad \overline{AB} \text{ (توسط) } \sigma_x \text{ (توسط) } \sigma_y \text{ (توسط) } \sigma_z \text{ (توسط)}$$

$$\overline{DE} = 4.5, \quad \bar{r} = 4.5, \quad R = \frac{h}{4} = 4.48, \quad e = \bar{r} - R = 0.02''$$

$$\sigma_x = \frac{My}{Ae(R-y)} = \frac{1100(0.48)}{(2)(0.2)(4)} = 3300 \text{ psi} \quad \overline{DE} \text{ (توسط) } \sigma_x \text{ (توسط) } \sigma_y \text{ (توسط) } \sigma_z \text{ (توسط)}$$

$$\sigma_x = \frac{1100(0.52)}{(2)(0.2)(5)} = 2860 \text{ psi} \quad \overline{BF} \text{ (توسط) } \sigma_x \text{ (توسط) } \sigma_y \text{ (توسط) } \sigma_z \text{ (توسط)}$$

$$\sigma_x = \frac{MC}{I} = \frac{1100 \times (0.5)}{(2)(11^3)/12} = 3300$$

استمال تفسیر

	X	Y	Z	
x'	λ_{x1}	λ_{y1}	λ_{z1}	$\lambda_{x1} = \cos(x, x')$
y'	λ_{x2}	λ_{y2}	λ_{z2}	
z'	λ_{x3}	λ_{y3}	λ_{z3}	$\lambda_{y1} = \cos(y, x')$

$$\sigma_{x'} = \sigma_x \lambda_{x1}^2 + \sigma_y \lambda_{y1}^2 + \sigma_z \lambda_{z1}^2 + 2(\bar{\tau}_{yz} \lambda_{y1} \lambda_{z1} + \bar{\tau}_{zy} \lambda_{z1} \lambda_{y1} + \bar{\tau}_{xz} \lambda_{x1} \lambda_{z1})$$

$$\begin{bmatrix} \sigma_{x'} & \tau_{x'y'} & \tau_{x'z'} \\ \tau_{y'x'} & \sigma_{y'} & \tau_{y'z'} \\ \tau_{z'x'} & \tau_{z'y'} & \sigma_{z'} \end{bmatrix} = \begin{bmatrix} \lambda_{x1} & \lambda_{y1} & \lambda_{z1} \\ \lambda_{x2} & \lambda_{y2} & \lambda_{z2} \\ \lambda_{x3} & \lambda_{y3} & \lambda_{z3} \end{bmatrix} \begin{bmatrix} \sigma_x & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_y & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \sigma_z \end{bmatrix} \begin{bmatrix} \lambda_{x1} & \lambda_{x2} & \lambda_{x3} \\ \lambda_{y1} & \lambda_{y2} & \lambda_{y3} \\ \lambda_{z1} & \lambda_{z2} & \lambda_{z3} \end{bmatrix}$$

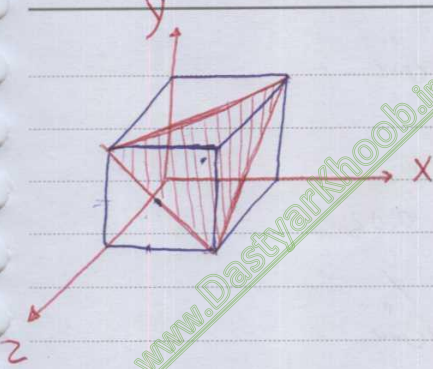


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$$[B_{xyz}] = \begin{bmatrix} 30 & 10 & 20 \\ 10 & 60 & 30 \\ 20 & 30 & 40 \end{bmatrix}$$

تاریخ اول :



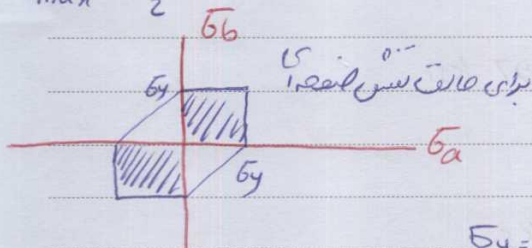
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قوانین تسلیم و شکست

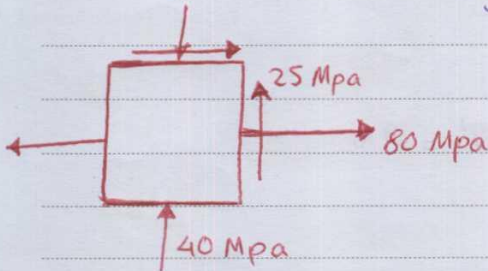
Tresca yield criteria

آزمایش به تنش برشی و کشش همزمان انجام می‌دهند. تنش تسلیم با ایند شکست متفاوت می‌باشد.

$$\tau_{max} \approx \frac{\sigma_y}{2}$$



مثال: $\sigma_y = 250 \text{ Mpa}$ ضریب ایمنی را مشخص کنید.



$$\sigma_{ave} = \frac{1}{2} (80 - 40) = 20 \text{ Mpa}$$

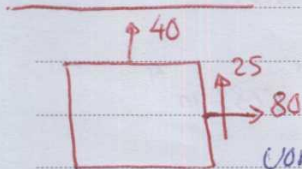
$$R = \sqrt{60^2 + 25^2} = 65$$

$$\sigma_a = 20 + 65 = 85$$

$$\sigma_b = 20 - 65 = -45$$

$$\frac{|\sigma_a - \sigma_b|}{\sigma_y} = \text{Tresca} \rightarrow \boxed{F.S. = 1.92}$$

$$\sigma_a^2 - \sigma_a \sigma_b + \sigma_b^2 = \left(\frac{\sigma_y}{F.S.}\right)^2 \xrightarrow{\text{von mises}} \boxed{F.S. = 2.19}$$



$$\sigma_a = 92 \quad \sigma_b = 28$$

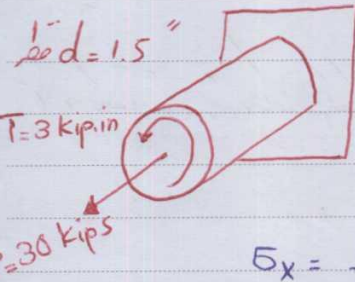
$$\text{von mises} \rightarrow (92)^2 - (92)(28) + (28)^2 = \left(\frac{250}{F.S.}\right)^2 \rightarrow F.S. = 3.06$$

$$\text{Tresca} \rightarrow F.S. = 2.72$$



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مثال: اگر $\sigma_y = 36$ باشد ضریب ایمنی را بر حسب روش تریساو

روش تریساو - von mises

$$\sigma_x = \frac{P}{A} = \frac{30 \times 10^3}{\frac{\pi (1.5)^2}{4}} = 16.97 \text{ ksi}$$

$$\tau = \frac{Tc}{J} = \frac{3 \times 10^3 \times (\frac{1.5}{2})}{0.5 \pi (\frac{1.5}{2})^4} = 4.53 \text{ ksi}$$

$$\sigma_{\text{ave}} = 8.48 \quad R = \sqrt{\left(\frac{16.97 - 0}{2}\right)^2 + (4.53)^2} = 9.6$$

$$\sigma_a = 18.08 \text{ ksi}$$

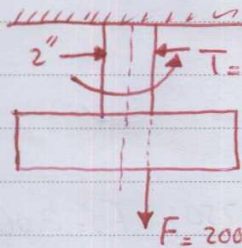
$$\sigma_b = -1.12 \text{ ksi} \quad \tau_{\text{max}} = \frac{1}{2} |18.08 + 1.12| = 9.6$$

$$F.S. \text{ تریساو} = \frac{18}{9.6} = 1.87$$

$$F.S. = 1.92$$

von mises

$$\sigma_a^2 - \sigma_a \sigma_b + \sigma_b^2 \leq \left(\frac{\sigma_y}{F.S.}\right)^2$$



مثال: $\sigma_y = 10 \text{ ksi}$ $\tau_y = 5 \text{ ksi}$

$$I_{\text{shaft}} = \frac{1}{4} \pi r^4 = \frac{\pi d^4}{64} = \frac{\pi (2)^4}{64} = 0.785 \text{ in}^4$$

$$J = \frac{I}{2} \times 2 = 1.57 \text{ in}^4$$



7.165, 7.97, 7.160, 7.161 ^{sy, 210}

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$$\sigma_x = \frac{P}{A} + \frac{Mc}{I} = \frac{2000}{\pi \cdot 2^2} + \frac{(2000 \times 1)(1)}{0.785} = 3180 \text{ psi}$$

Handwritten signature

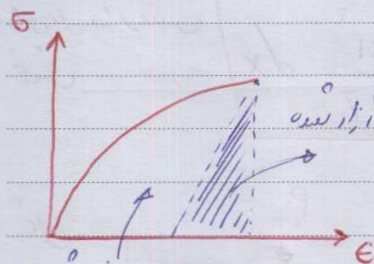
$$\tau_{xy} = \frac{Tc}{J} = \frac{(1600)(1)}{1.57} = 637 \text{ psi}$$

$$\sigma_a = \left(\frac{3180}{2} \right) + \sqrt{\left(\frac{3180}{2} \right)^2 + (637)^2} = 3305 \text{ psi}$$

$$\sigma_{min} = -122 \text{ psi}$$

$$F.S. \text{ factor} = \frac{\tau_y}{\tau_{max}} = \frac{5000}{1713.5}$$

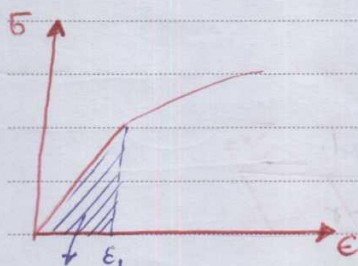
$$\text{von mises} \rightarrow (3305)^2 + (122)(3305) + 122^2 = \left(\frac{10000}{F.S.} \right)^2 \rightarrow F.S.$$



روش انرژی

$$U = \frac{U}{AL} = \int_0^x \frac{P}{A} \frac{dx}{L} = \int \sigma d\epsilon$$

انرژی برای تغییر شکل



$$U = \int_0^{\epsilon_1} \sigma_x d\epsilon_x \Rightarrow \frac{E \epsilon_1^2}{2} = \frac{\sigma_1^2}{2E} = \frac{1}{2} \sigma \epsilon$$

$$U = \int_0^{\epsilon_x} \sigma_x d\epsilon_x = \frac{\sigma_x^2}{2E} = \frac{1}{2} \sigma_x \epsilon_x$$

Module of Resilience
 U_y

$$U = \int_0^V \frac{\sigma_x^2}{2E} dV$$

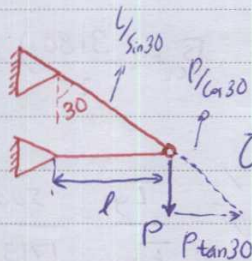
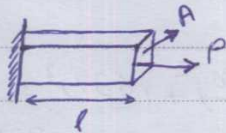
Handwritten notes: $\frac{P}{A}$, $\frac{My}{I}$, and other terms related to stress and strain.



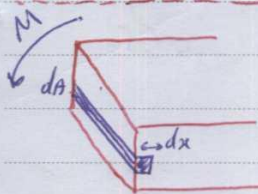
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$$\sigma_x = \frac{P}{A} \quad U = \int \frac{P^2}{2A^2E} A dx = \int \frac{P^2}{2AE} dx \quad \frac{A}{\text{برابر}} \quad \frac{P^2 L}{2AE} \quad \begin{matrix} \text{انرژی کل در اثر} \\ \text{بار محوری} \end{matrix}$$



$$U = \frac{1}{2} \frac{(P \cos 30)^2 (L / \sin 30)}{2AE} + \frac{1}{2} \frac{(P \sin 30)^2 L}{2AE} = \frac{1.5 PL^2}{AE}$$



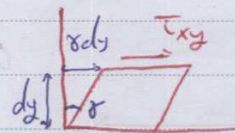
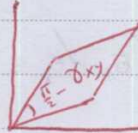
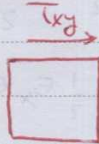
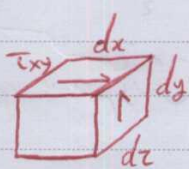
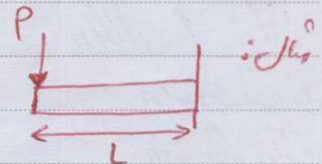
$$\sigma = \frac{My}{I}$$

$$U = \int \frac{M y^2}{2EI^2} dV \quad \frac{dV = dA \cdot dx}{}$$

$$U = \int \frac{M^2}{2EI^2} \left(\int y^2 dA \right) dx \Rightarrow U = \int \frac{M^2}{2EI} dx$$

$$M = -Px$$

$$U = \int \frac{Px^2}{2EI} dx = \frac{PL^3}{6EI}$$



$$U_{\tau} = \frac{1}{2} (\delta dy) (\tau dx dz) = \frac{1}{2} \tau_{xy} \delta dx dy dz$$

$$U = \frac{1}{2} \delta \tau_{xy} = \frac{\tau_{xy}^2}{2G} = \frac{1}{2} G \delta^2$$

$$\tau_{xy} = G \delta$$

$$G = \frac{E}{2(1+\nu)}$$

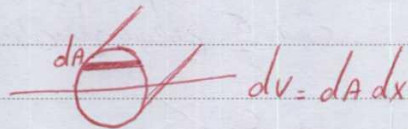
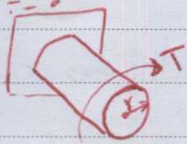


11. 34, 20, 11, 13

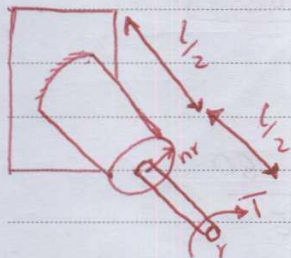
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تغییر انرژی در اثر تنش:
$$U = \int_0^V \frac{\tau_{xy}}{2G} dV = \int \frac{T r^2}{2GJ^2} dV$$



$$U = \int_0^L \frac{T}{2GJ^2} \left(\int r^2 dA \right) dx \rightarrow U = \int_0^L \frac{T}{2GJ} dx = \boxed{\frac{T^2 L}{2GJ}}$$

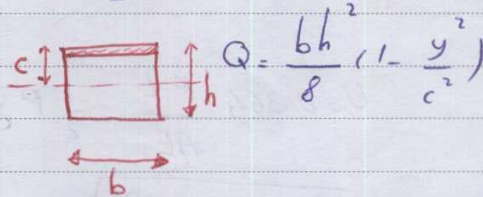
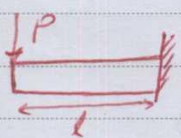


مثال:

$$J_1 = \frac{\pi r^4}{2} \quad J_2 = n^4 \frac{\pi r^4}{2} = n^4 J_1$$

$$U = \frac{T^2 L/2}{2GJ_1} + \frac{T^2 L/2}{2n^4 GJ_1} \rightarrow U = \frac{T^2 L/2}{2GJ_1} \left(1 + \frac{1}{n^4} \right)$$

تغییر انرژی در اثر نیروی برشی:
$$\tau = \frac{VQ}{It}$$



$$\tau_{xy} = \frac{3}{2} \frac{P}{bh} \left(1 - \frac{y^2}{c^2} \right) \quad U = \int_0^V \frac{\tau_{xy}}{2G} dV = \frac{1}{2G} \left(\frac{3}{2} \frac{P}{bh} \right)^2 \int_0^V \left(1 - \frac{y^2}{c^2} \right) dV$$

در نهایت:

$$\boxed{\frac{U}{P} = \frac{3}{5} \frac{P^2 L}{GA}}$$

تغییرات در انرژی دریاک در نوع انرژی U_T و U_σ دارد

$$U_\sigma = \frac{P^2 L^3}{6EI}$$

با جمع مع من شوند

P4PCO

$$U = U_T + U_\sigma = U_\sigma \left(1 + \frac{3Eh^2}{10GL^2} \right)$$



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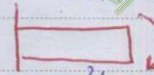
$$U = \int \alpha \frac{P^2}{2GA} dx$$

حالت پس انرژی کشش از نیروی برشی α در یک مقطع ثابت

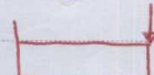
است و در عنوان مثال برای مقطع مستطبی $\alpha = \frac{5}{8}$ است



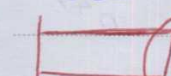
$$U = \frac{P^2 L}{2AE} = \frac{1}{2} P \Delta x$$



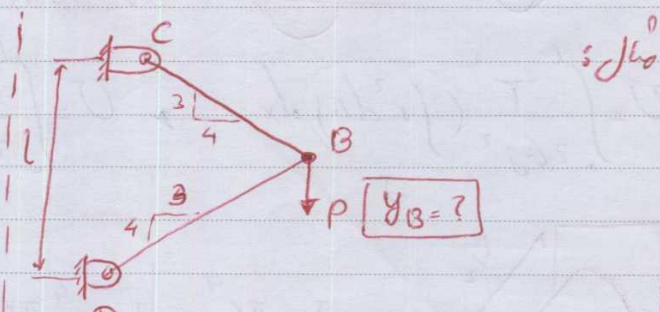
$$U = \frac{M^2 L}{2EI} = \frac{1}{2} M \Delta \theta$$



$$U = \frac{P^2 L^3}{6EI} = \frac{1}{2} P \Delta y$$



$$U = \frac{T^2 L}{2GJ} = \frac{1}{2} T \Delta \phi$$



$$U = \frac{F_{BC}^2 \times BC}{2AE} + \frac{F_{BD}^2 \times BD}{2AE}$$

$$F_{BC} = 0.6P \quad F_{BD} = 0.8P$$

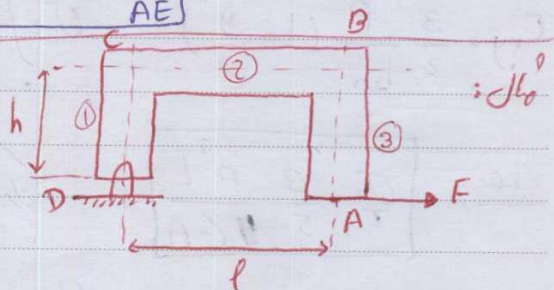
$$BC = 0.6L \quad BD = 0.8L$$

$$U = 0.364 \frac{P^2 L}{AE} = \frac{1}{2} P y_B$$

$$y_B = 0.726 \frac{PL}{AE}$$

$$W = \frac{1}{2} F \Delta x_A$$

$$U_3 = \frac{F^2 h^3}{6EI}$$

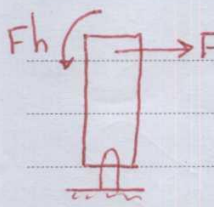


$$U_2 = \frac{(F^2 h^2) L}{2EI} + \frac{F^2 L}{2AE}$$



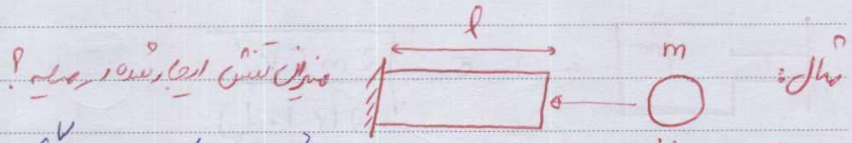
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$$U_1 = \frac{F^2 h^3}{6EI}$$

$$W = U_1 + U_2 + U_3 \rightarrow \Delta x = \frac{2Fh^3}{3EI} + \frac{Fh^2 l}{EI} + \frac{Fl}{AE}$$

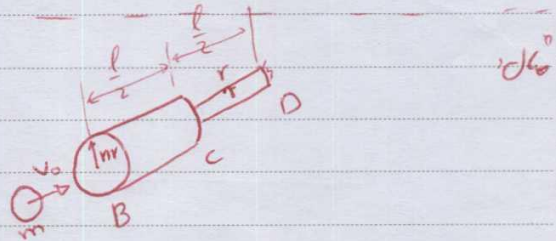


$$U_m = \frac{1}{2} m v_0^2 = \int_0^l \frac{1}{2} (\sigma E) dV = \frac{\sigma_m^2 V}{2E}$$

سرعت اولیه را به منظور استفاده

$$\sigma_m = \sqrt{\frac{m v_0^2 E}{V}}$$

$$\sigma_{CD} = \sigma_m \quad A_{BC} = n^2 A_{CD}$$

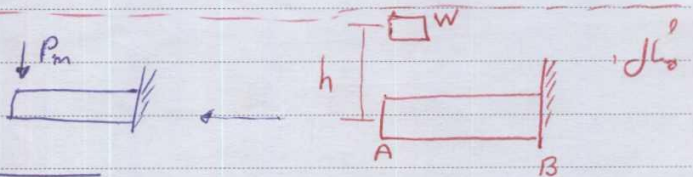


$$\sigma_{BC} = \frac{1}{n^2} \sigma_m$$

$$U_m = \frac{(\sigma_{CD})^2 V_{CD}}{2E} + \frac{(\sigma_{BC})^2 V_{BC}}{2E} = \frac{1}{2E} (\sigma_m^2) \frac{Al}{2} + \frac{1}{2E} \left(\frac{1}{n^2} \sigma_m\right)^2 \left(\frac{n^2 Al}{2}\right)$$

$$\frac{\sigma_m^2 Al}{4E} \left(1 + \frac{1}{n^2}\right) = \frac{1}{2} m v_0^2 \rightarrow \sigma_m = \sqrt{\frac{2mE v_0^2}{Al \left(1 + \frac{1}{n^2}\right)}}$$

$$U_m = Wh$$



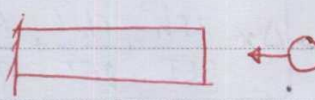
$$U_m = \frac{P_m^2 L^3}{6EI} \quad P_m = \sqrt{\frac{6U_m EI}{L^3}}$$

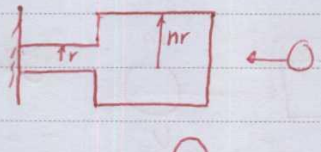
$$\sigma = \frac{(P_m L) C}{I} = \sqrt{\frac{6U_m E}{L \left(I_{z2}\right)}}$$

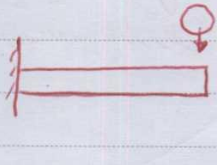


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$$\sigma_m = \sqrt{\frac{2 U_m E}{V}}$$


$$\sigma_m = \sqrt{\frac{2 m E V_0^2}{A \left(1 + \frac{l}{n^2}\right)}}$$


$$\sigma_m = \sqrt{\frac{6 U_m E}{L \left(\frac{I}{I_0}\right)}}$$

برای مقادیر مختلف نیروها:

1! سعی شود که تنش بصورت یکنواخت توزیع گردد.

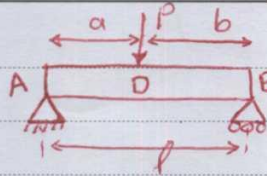
2- که از E کمتر استفاده شود.

3- که V بیشتر



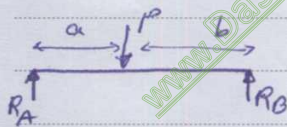
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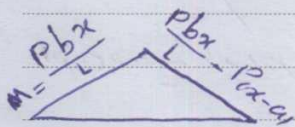


W10x45 $\Rightarrow I = 248 \text{ in}^4$ $P = 40 \text{ kips}$ سوال:
 $a = 3 \text{ ft}$ $b = 9 \text{ ft}$ $E = 2.9 \times 10^6 \text{ psi}$ $y_D = ?$

از اثر نیروی کششی صرف نظر کنیم. (بهتر است از این قابل استفاده است)



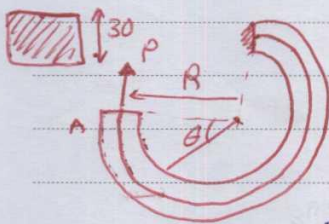
$$R_A = \frac{Pb}{L} \quad R_B = \frac{Pa}{L}$$



$$U = U_{AD} + U_{DB} = \int_0^a \left(\frac{Pbx}{L} \right)^2 dx + \int_a^L \left(\frac{Pbx}{L} - P(x-a) \right)^2 dx$$

$$U = \frac{P^2 a^2 b^2}{2EI L^2} (a+b) = \frac{(40)^2 (36)^2 (108)^2}{6(29 \times 10^3)(248)(144)} = 3.89 \text{ (in)(k/lb)}$$

$$\frac{1}{2} (40) y_D = 3.89 \rightarrow y_D = 0.1945''$$



$R = 65 \text{ mm}$ $E = 200 \text{ GPa}$ $\nu = 0.29$

$P = 6 \text{ kN}$ $y_A = ?$ در این سوال از اثر کششی صرف نظر کردیم

$$M = PR(1 - \cos \theta) \quad N = P \cos \theta \quad V = P \sin \theta$$

$$dx = R d\theta \quad U = \int_0^{\frac{3\pi}{2}} \frac{M^2}{2EI} R d\theta + \int_0^{\frac{3\pi}{2}} \frac{(P \cos \theta)^2}{2AE} R d\theta + \frac{3}{5} \int_0^{\frac{3\pi}{2}} \frac{(P \sin \theta)^2}{GA} R d\theta$$

$$G = \frac{E}{2(1+\nu)} = 77.5 \text{ GPa}$$

$$U = \frac{1}{2} \frac{P^2 R^3}{EI} \int_0^{\frac{3\pi}{2}} \left(1 - 2 \cos \theta + \frac{1}{2} + \frac{1}{2} \cos 2\theta \right) d\theta$$

PAPCO

$$U = \int_0^{\frac{3\pi}{2}} \frac{10^2 R^3}{2AE} \left(\frac{1}{2} + \frac{1}{2} \cos 2\theta \right) d\theta$$

$$M = PR(1 - \cos \theta) = RP(1 + \cos^2 \theta - 2 \cos \theta)$$

$$\cos^2 \theta = \frac{1}{2} + \frac{1}{2} \cos 2\theta$$



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$$U = \frac{3PR^2}{5GA} \int_0^{\frac{3\pi}{2}} \left(\frac{1}{2} - \frac{1}{2} \cos 2\theta \right) d\theta$$

$$U = \frac{PR^2}{2EI} \left(\frac{9\bar{u} + 8}{4} \right) + \frac{PR^2}{2AE} \left(\frac{3\bar{u}}{4} \right) + \frac{3PR^2}{5GA} \left(\frac{3\bar{u}}{4} \right)$$

$$\frac{1}{2} y \times P = U \rightarrow \boxed{y = \frac{2U}{P}}$$

انرژی همبند باید درین سیستم معادله شود نه درین نقطه خاص. ^{مستند در اینجا}

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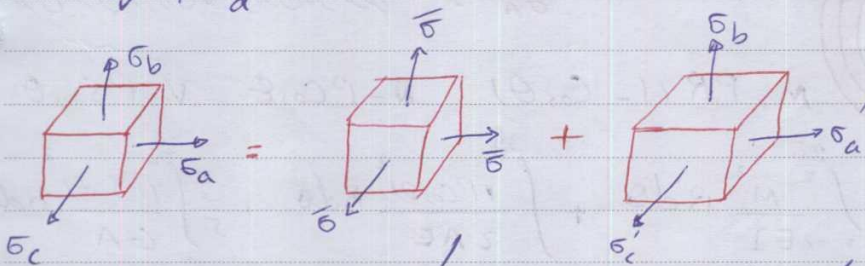
صفت کلی انرژی:

$$U = \frac{1}{2E} [\sigma_x^2 + \sigma_y^2 + \sigma_z^2 - 2\nu(\sigma_x\sigma_y + \sigma_y\sigma_z + \sigma_z\sigma_x)] + \frac{1}{2G} \left[\tau_{xy}^2 + \tau_{xz}^2 + \tau_{yz}^2 \right]$$

در معادله های اصلی اینها نسبت به هم دارند - هم در این است:

$$U = \frac{1}{2E} [\sigma_a^2 + \sigma_b^2 + \sigma_c^2 - 2\nu(\sigma_a\sigma_b + \sigma_b\sigma_c + \sigma_c\sigma_a)]$$

$$U = U_v + U_d$$



$$\bar{\sigma} = \frac{\sigma_a + \sigma_b + \sigma_c}{3} \quad \sigma_a' + \sigma_b' + \sigma_c' = 0$$

$$\frac{\Delta V}{V} = \frac{1-2\nu}{E} (\sigma_a' + \sigma_b' + \sigma_c') = 0$$

P4PCO

و تغییر حجم انسی از σ می باشد. تاثیر σ ها، $distorsion$ می باشد.



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انرژی مربوط به تغییر حجم

$$U_v = \frac{3(1-2\nu)\bar{\sigma}^2}{2E} = \frac{1-2\nu}{6E} (\sigma_a + \sigma_b + \sigma_c)^2$$

انرژی مؤلفه تنش $\bar{\sigma}$ با قرار دهیم انرژی را بر حسب این روش:

انرژی مربوط به تغییر شکل

$$U_d = U - U_v = \frac{1+\nu}{6E} [(\sigma_a - \sigma_b)^2 + (\sigma_b - \sigma_c)^2 + (\sigma_c - \sigma_a)^2]$$

در حالت تنش لنگری

$$U_d = \frac{1}{6G} [\sigma_a^2 - \sigma_a\sigma_b + \sigma_b^2]$$

$\sigma_c = 0$

در حالت تنش لنگری

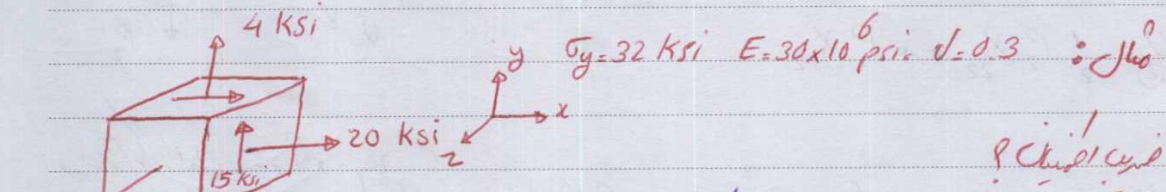
$$\sigma_a = \sigma_y \quad \sigma_b = \sigma_c = 0 \rightarrow U_d = \frac{\sigma_y^2}{6G} \rightarrow \sigma_a^2 - \sigma_a\sigma_b + \sigma_b^2 < \sigma_y^2$$

در حالت سه محوری

$$(\sigma_a - \sigma_b)^2 + (\sigma_b - \sigma_c)^2 + (\sigma_c - \sigma_a)^2 < 2\sigma_y^2$$

معیار انژی برای تسلیم

این معیار مربوط به استوانه با شیب $\sqrt{\frac{2}{3}}$ است که از مبدأ مختصات میگذرد.



انتخاب کنید تنش ها اصلی را بیابیم برای این کار باید در مختصات ماکزیمم در هر دو محور هم باشد.

$$\begin{vmatrix} 20-\sigma & 15 & 0 \\ 15 & 4-\sigma & 0 \\ 0 & 0 & 9-\sigma \end{vmatrix} = 0 \rightarrow (20-\sigma)(4-\sigma)(9-\sigma) - 225(9-\sigma) = 0$$

$\sigma_c = 9 \quad \sigma_b = 5 \quad \sigma_a = 29$

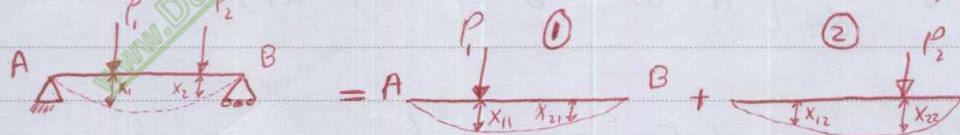


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$$(29-9)^2 + (29-5)^2 + (9-5)^2 = 992 \quad 25y^2 = 2048$$

$$F.S = \sqrt{\frac{2048}{992}}$$



in ① $X_{11} = \alpha_{11} P_1$

in ② $X_{12} = \alpha_{12} P_2$

$$X_{21} = \alpha_{21} P_1$$

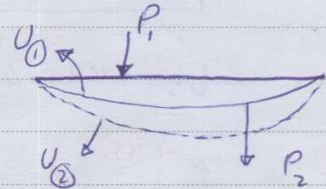
$$X_{22} = \alpha_{22} P_2$$

$$X_1 = X_{11} + X_{12} = \alpha_{11} P_1 + \alpha_{12} P_2$$

$$U = U_{(1)} + U_{(2)}$$

$$X_2 = X_{21} + X_{22} = \alpha_{21} P_1 + \alpha_{22} P_2$$

$$U_{(1)} = \frac{1}{2} P_1 X_{11} = \frac{1}{2} P_1 (\alpha_{11} P_1) = \frac{1}{2} \alpha_{11} P_1^2$$



$$U_{(2)} = \frac{1}{2} P_2 X_{22} + P_1 X_{12}$$

$$U = U_{(1)} + U_{(2)} = \frac{1}{2} [\alpha_{11} P_1^2 + 2\alpha_{12} P_1 P_2 + \alpha_{22} P_2^2]$$

در حالت اول فقط P_1 داریم و P_2 نداریم!
در حالت دوم اول P_2 داریم و P_1 را وارد کنیم

$$U = U_{(1)} + U_{(2)} = \frac{1}{2} [\alpha_{11} P_1^2 + 2\alpha_{21} P_1 P_2 + \alpha_{22} P_2^2]$$

در حالت اول فقط P_2 داریم و P_1 را وارد کنیم
در حالت دوم اول P_1 داریم و P_2 را وارد کنیم

$$\alpha_{12} = \alpha_{21}$$

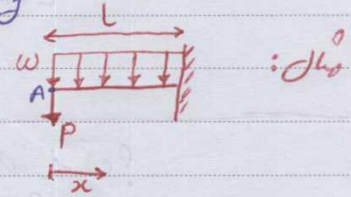


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$$\frac{\partial U}{\partial P_1} = \alpha_{11} P_1 + \alpha_{12} P_2 = X_1 \quad \frac{\partial U}{\partial P_2} = \alpha_{11} P_1 + \alpha_{12} P_2 = X_2$$

$$\frac{\partial U}{\partial M_j} = \theta_j \quad \frac{\partial U}{\partial T_j} = \phi_j \quad \text{فرض } j \text{ فرضی } = \frac{\partial U}{\partial F_j} = \delta_j \text{ فرضی}$$

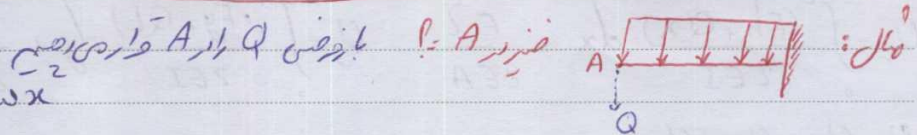
$$U = \int_0^L \frac{M^2}{2EI} dx \quad M = +Px + \frac{1}{2}wx$$



$$y_A = \frac{\partial U}{\partial P} = \frac{\partial U}{\partial M} \times \frac{\partial M}{\partial P} = \int_0^L \frac{M}{EI} dx$$

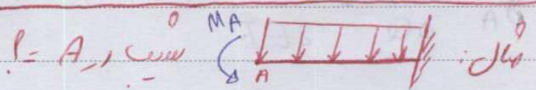
$$y_A = \int_0^L \frac{M}{EI} (x) dx = \int_0^L \frac{1}{EI} [Px + \frac{1}{2}wx^2] (1) dx = \frac{1}{EI} \left(\frac{PL^3}{3} + \frac{wL^4}{8} \right)$$

$$M = Qx + \frac{1}{2}wx$$



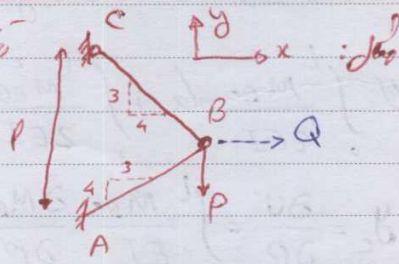
$$\frac{\partial U}{\partial Q} = \int_0^L (Qx + \frac{1}{2}wx^2) (1) dx = \frac{wL^4}{8EI}$$

$$M = M_A + \frac{1}{2}wx^2$$



$$\frac{\partial U}{\partial M_A} = \frac{\partial U}{\partial M} \frac{\partial M}{\partial M_A} = \int_0^L (M_A + \frac{1}{2}wx^2) (1) dx = \frac{wL^3}{6EI}$$

$$U = \frac{F_{BC}^2 (BC)}{2EA} + \frac{F_{AB}^2 (AB)}{2EA}$$



$$X_B = \frac{\partial U}{\partial Q} = \frac{F_{BC} (BC)}{EA} \frac{\partial F_{BC}}{\partial Q} + \frac{F_{AB} (AB)}{EA} \frac{\partial F_{AB}}{\partial Q}$$



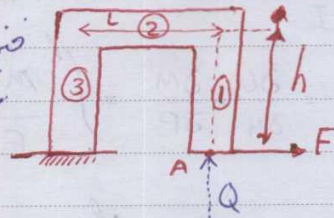
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$$F_{AB} = -0.8P + 0.6Q \quad F_{BC} = 0.6P + 0.8Q$$

$$Q=0 \rightarrow X_B = \frac{(0.6P)(0.6l)(0.8)}{EA} + \frac{(-0.8P)(0.8l)(0.6)}{EA} = -0.096 \frac{PL}{EA}$$

علاقت بین نیروی خارجی و نیروی داخلی Q برآید.

فرض کنیم عمودی از نقطه A لغزناپذیر است؟
 فرض کنیم افقی



$$U_1 = \int_0^h \frac{(Fy)^2}{2EI} dy + \frac{Q^2 h}{2EA}$$

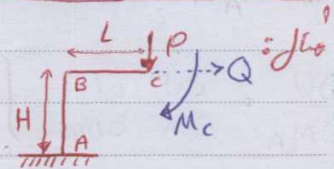
$$U_2 = \int_0^L \frac{(Fh + Qx)^2}{2EI} dx + \frac{F^2 L}{2EA} \quad U_3 = \int_0^h \frac{(Fy + QL)^2}{2EI} dy + \frac{Q^2 h}{2EA}$$

$$U = U_1 + U_2 + U_3$$

$$y_A = \frac{\partial U}{\partial Q} = \frac{FLh}{2EI} (L+h) \quad x_A = \frac{\partial U}{\partial F} = \frac{Fh^2}{EI} \left(\frac{2h}{3} + L \right)$$

$x_c, y_c, \theta_c = ?$

BC: $M = Px + M_c$
 AB: $M = PL + Qy + M_c$



$$U = \int_0^L \frac{M_{BC}^2}{2EI} dx + \int_0^H \frac{M_{AB}^2}{2EI} dy + \frac{P^2 H}{2EA} + \frac{Q^2 L}{2EA}$$

$$y_c = \frac{\partial U}{\partial P} = \int_0^L \frac{M_{BC}}{EI} \frac{\partial M_{BC}}{\partial P} dx + \int_0^H \frac{M_{AB}}{EI} \frac{\partial M_{AB}}{\partial P} dy + \frac{PH}{EA}$$



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$$y_c = \frac{\partial U}{\partial P} = \int_0^L \frac{(Px + M_c) x}{EI} dx + \int_0^H \frac{PL + Qy + M_c}{EI} (1) dy + \frac{PH}{EA}$$

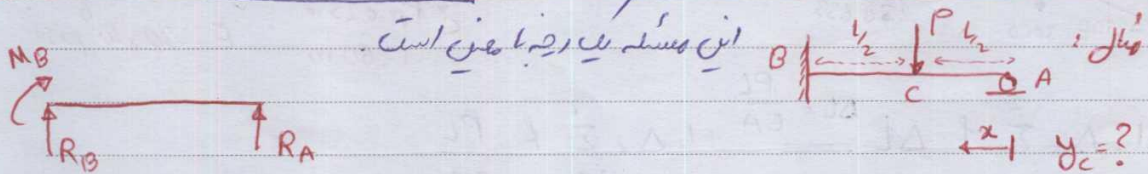
$$\boxed{y_c = \frac{PL^3}{3EI} + \frac{PLH}{EI} + \frac{PH}{EA}}$$

$$x_c = \frac{\partial U}{\partial Q} = \int_0^L \frac{Px + M_c}{EI} (0) dx + \int_0^H \frac{PL + Qy + M_c}{EI} y dy + 0$$

$$\boxed{x_c = \frac{PLH^2}{2EI}}$$

$$\theta_c = \frac{\partial U}{\partial M_c} = \int_0^L \frac{Px + M_c}{EI} (1) dx + \int_0^H \frac{PL + Qy + M_c}{EI} (1) dy$$

$$\boxed{\theta_c = \frac{PL^2}{2EI} + \frac{PLH}{EI}}$$



$$M = R_A x \quad 0 \leq x \leq \frac{l}{2}$$

$$U = \int_0^{\frac{l}{2}} \frac{(R_A x)^2}{2EI} dx + \int_{\frac{l}{2}}^l \frac{[R_A x - P(x - \frac{l}{2})]^2}{2EI} dx$$

$$M = R_A x - P(x - \frac{l}{2}) \quad \frac{l}{2} \leq x \leq l$$

$$\frac{\partial U}{\partial R_A} = \int_0^{\frac{l}{2}} \frac{R_A x^2}{EI} dx + \int_{\frac{l}{2}}^l \frac{[R_A x - P(x - \frac{l}{2})] x}{EI} dx$$

$$\frac{\partial U}{\partial R_A} = \frac{R_A}{3} \left(\frac{l}{2}\right)^3 + \frac{R_A}{3} \left[l^3 - \left(\frac{l}{2}\right)^3\right] - \frac{P}{3} \left[l^3 - \left(\frac{l}{2}\right)^3\right] + \frac{PL}{4} \left[l^3 - \left(\frac{l}{2}\right)^3\right] = 0$$



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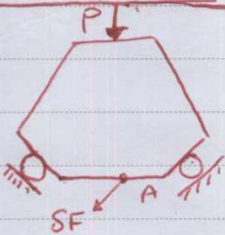
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$$R_A = \frac{5P}{16}$$

چون در نقطه A بارهای ثابت و متغیر داریم و در نقطه A هم بار داریم پس $\frac{\partial U}{\partial R_A} = 0$ می‌باشد.

$$y_c = \frac{\partial U}{\partial P} = \frac{\partial}{\partial P} \left[\int_0^{L/2} \frac{(Rx)^2}{2EI} dx + \int_{L/2}^L \frac{[Rx - P(x - \frac{L}{2})]^2}{2EI} dx \right]$$

$$= \int_{L/2}^L \frac{P - (x - \frac{L}{2})(Rx - P(x - \frac{L}{2}))}{EI} dx \rightarrow y_c = \frac{7}{768} \frac{PL^3}{EI}$$

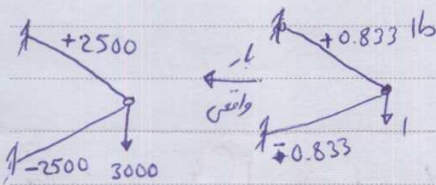


$$SF \cdot \Delta = \sum SF \cdot \Delta L$$

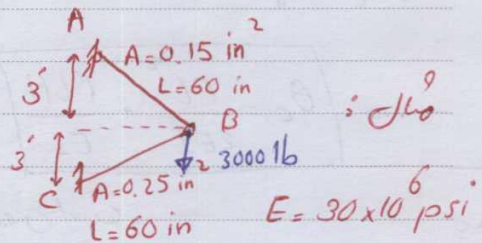
$$I \cdot \Delta = \sum f \cdot \Delta L$$

Virtual Work

Force Method (Unit Load)



والب



$$I \cdot \Delta = \sum_{i=1}^2 f \cdot \Delta L \quad \Delta L = \frac{PL}{EA} \quad I \cdot \Delta = \sum_{i=1}^2 f \cdot \frac{PL}{EA}$$

	f	P	L	A
AB	+0.833	2500	60	0.15
BC	-0.833	-2500	60	0.25

$$I \cdot \Delta = \frac{f_{AB} P_{AB} L_{AB}}{E A_{AB}} + \frac{f_{BC} P_{BC} L_{BC}}{E A_{BC}} = +0.0444 \text{ in}$$

مختصر طول B (تغییر طول) (تغییر طول)

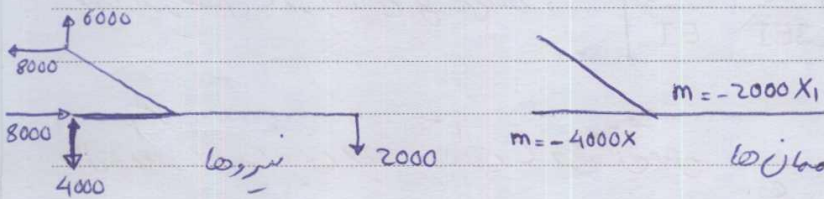
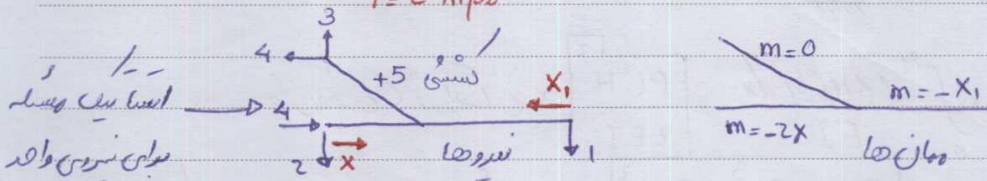
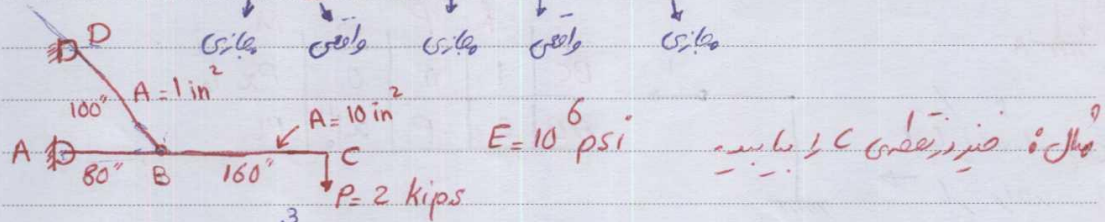


Virtual Work • Force Method Unit Load

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$$\delta F \cdot \Delta = \sum \delta F \cdot \Delta L + \sum \delta m \cdot \Delta \theta$$

$$1 \cdot \Delta = \sum F \cdot \Delta L + \sum m \cdot \Delta \theta$$



$$1 \times \Delta = \sum F \frac{PL}{EA} + \sum \int_0^L m \frac{M dx}{EI} = \frac{F_{AB} P_{AB} L_{AB}}{E A_{AB}} + \frac{F_{BC} P_{BC} L_{BC}}{E A_{BC}} + \frac{F_{DB} P_{DB} L_{DB}}{E A_{DB}}$$

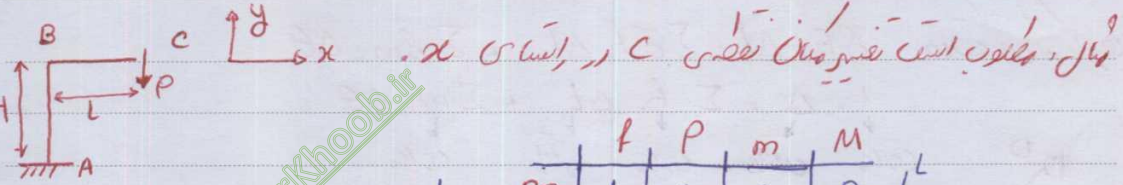
$$+ \int_0^{80} \frac{m_{AB} M_{AB} dx_{AB}}{EI} + \int_0^{160} \frac{m_{BC} M_{BC} dx_{BC}}{EI}$$

	F	P	L	A	m	M
AB	-4	-8000	80	10	$-2x \Big _0^{80}$	$-4000 \Big _0^{80}$
BC	0	0	160	10	$-x_1 \Big _0^{160}$	$-2000 \Big _0^{160}$
BD	5	10000	100	1	0	0

نتیجه محاسبه: $1 \times \Delta = 2.92 \text{ in}$



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	f	P	m	M
BC	1	0	0	$Px \frac{L}{EI}$
AB	0	-P	$x \frac{H}{EI}$	PL

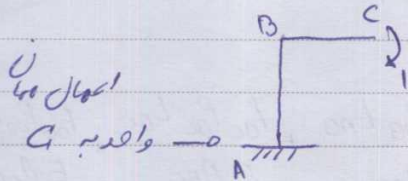
$$1 \times \Delta = 0 + \int_0^H \frac{1(x)(PL)}{EI} dx = \frac{PLH^2}{2EI}$$

خ راستی C، زیر نیروی 1

$$\frac{PH}{EA} + \frac{PL^3}{3EI} + \frac{PHL^2}{EI}$$

نسبتاً زیر نیروی C، راستی y در راستی 1

سوال: معلوم است چقدر است چرخش در نقطه C، در سؤال قبل



	f	P	m	M
BC	0	0	1	$Px \frac{L}{EI}$
AB	0	-P	1	PL

$$1 \times \Delta = 0 + 0 + \int_0^L \frac{1(x)(Px)}{EI} dx + \int_0^H \frac{1(x)(PL)}{EI} dx = \frac{PL^2}{2EI} + \frac{PLH}{EI}$$

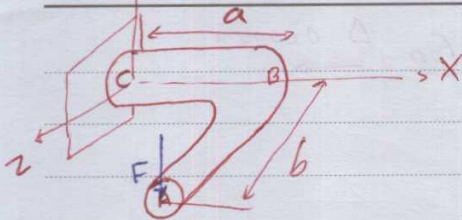
* زاویه چرخش در نقطه C چقدر است.

در حالتی که لنگر و نیروی هم راسته باشند، رابطه‌ی زیر برقرار است:

$$1 \times \Delta = \sum f \cdot \Delta_L + \sum \int_0^L \frac{m M dx}{EI} + \sum \int_0^L \frac{T dx}{GJ}$$



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پهلو: غیر برقی A

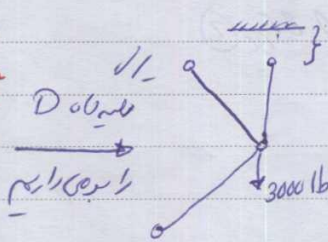
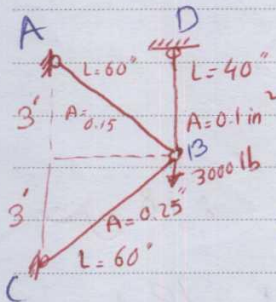
با استفاده از روش انرژی قبل از تغییر شکل

	L	f	P	m	M	t	T
AB	b	0	0	Z ₀ ^b	Fz ₀ ^b	0	0
BC	a	0	0	x ₀ ^a	Fx ₀ ^a	b	Fb

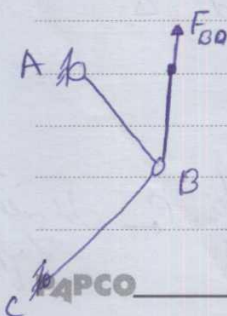
$$1 \times \Delta = \frac{F_{AB} P_{AB} L_{AB}}{E A_{AB}} + \frac{F_{BC} P_{BC} L_{BC}}{E A_{BC}} + \int_0^b \frac{m_{AB} M_{AB}}{EI} dz + \int_0^a \frac{m_{BC} M_{BC}}{EI} dx + \int_0^b \frac{t_{AB} T_{AB}}{GJ} dx + \int_0^a \frac{t_{BC} T_{BC}}{GJ} dx$$

$$1 \times \Delta = \int_0^b \frac{(z)(Fz)}{EI} dz + \int_0^a \frac{(x)(Fx)}{EI} dx + \int_0^a \frac{(b)(Fb)}{GJ} dx$$

$$\Delta = \frac{Fb^3}{3EI} + \frac{Fa^3}{3EI} + \frac{Fb^2 a}{GJ}$$



نتیجه:



	L	A	f	F
AB	60	0.15	-0.833	-0.833 F _{BD}
BC	60	0.25	0.833	0.833 F _{BD}
BD	40	0.1	1	F _{BD}



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$$1. \Delta = \frac{\sum f FL}{EA} = \frac{278 F_{BD} + 167 F_{BD} + 400 F_{BD}}{E} \rightarrow \Delta = 0.0444 \text{ in}$$

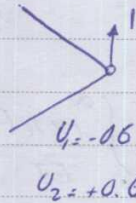
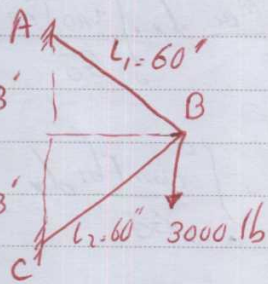
$$\rightarrow F_{BD} = 1576 \text{ lb}$$

Displacement Methods

برای روش هدف برسی اولین نیروها است.

$$1 \times P = \sum u_i \times F_i$$

واری *واری*

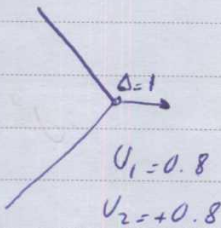


$$u_1 = -0.6 \quad (1)(-3000) = -0.6 F_{AB} + 0.6 F_{BC} \quad (1)$$

$$u_2 = +0.6$$

سوال: چطوری است نیروها را می.

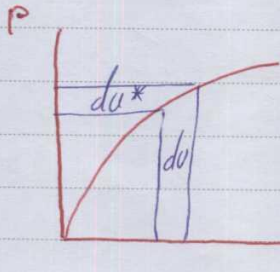
بعد فرضین 1, 2) F_{BC} F_{AB} برسی می.



$$(1)(0) = 0.8 F_{AB} + 0.8 F_{BC} \quad (2)$$

$$u_1 = 0.8$$

$$u_2 = +0.8$$



فصل 18

$$dw = du = P \cdot \Delta L$$

$$dw^* = du^* = dP \cdot \Delta$$

$$\frac{du}{d\delta} = P$$

$$\frac{du^*}{dP} = \Delta$$

Linear system of loading $\rightarrow w^* = w, U^* = U, \frac{du}{d\delta} = P$ *فصل اول*

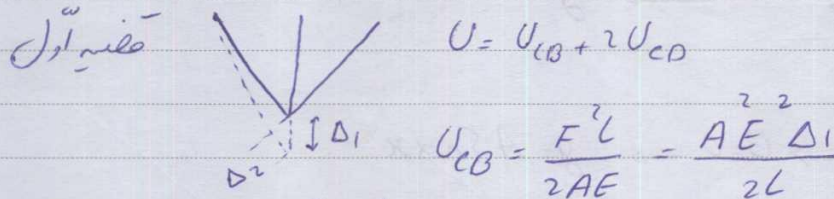
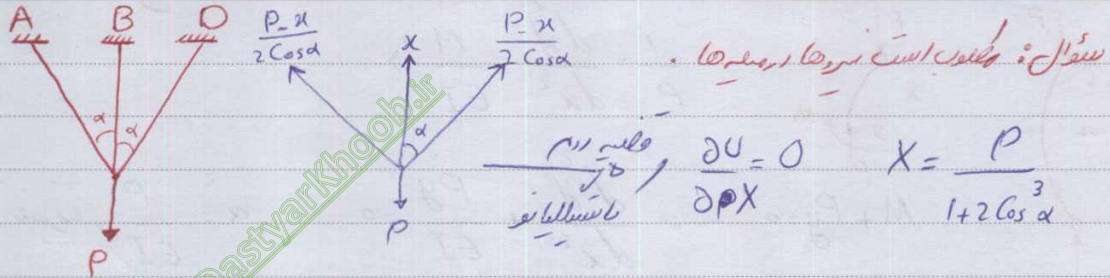
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$$\frac{dw}{dP} = \frac{du}{dP} = \Delta \leftarrow \text{فصل اول}$$



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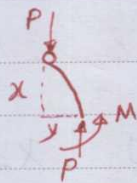
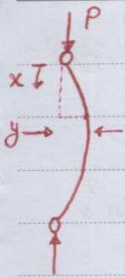


$$U = \frac{AE \Delta_1^2}{2L} + 2 \frac{AE \Delta_1^2 \cos^3 \alpha}{2L}$$
$$\frac{\partial U}{\partial \Delta} = P \quad \Delta = \frac{PL}{EA} \times \frac{1}{1+2\cos^3 \alpha}$$



لغزش Buckling

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$$\frac{1}{P} = \frac{d^2 y}{dx^2} = \frac{M}{EI} \Rightarrow$$

$$M + Py = 0 \rightarrow \frac{d^2 y}{dx^2} + \frac{Py}{EI} = 0 \quad \alpha^2 = \frac{P}{EI}$$

$$\rightarrow \frac{d^2 y}{dx^2} + \alpha^2 y = 0 \xrightarrow{\text{حل}} y = A \sin \alpha x + B \cos \alpha x$$

شرایط مرزی $\begin{cases} x=0 \\ y=0 \end{cases} \Rightarrow B=0 \rightarrow y = A \sin \alpha x$

قالب قبول نیست $\begin{cases} x=L \\ y=0 \end{cases} \Rightarrow \begin{cases} A=0 \\ \sin \alpha x = 0 \end{cases} \rightarrow \alpha L = n\pi \rightarrow \boxed{P = \frac{n^2 \pi^2 EI}{L^2}}$

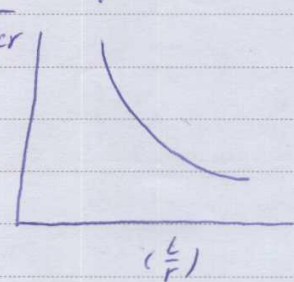
در عمل $n=1$ سروتن، بار کم و حالت بحرانی برای n یعنی اول است. $\boxed{P_{cr} = \frac{\pi^2 EI}{L^2}}$

* تا قبل از نیروی بحرانی (تیر استوار) هیچ تغییر شکل ناگهانی و طارقاتی اتفاق نمی‌افتد. نیروی بحرانی P_{cr}

لا مارتین نیست هرچنین $y_{max} = A$ البته مقدار A را نمی‌توانیم بر حسب σ تعیین کنیم.

$$\sigma_{cr} = \frac{\pi^2 EI / A}{L^2} \quad I = Ar^2 \rightarrow \sigma_{cr} = \frac{\pi^2 E}{\left(\frac{L}{r}\right)^2}$$

ریشه اول σ_{cr} = σ_{cr} = شعاع تیر استوار است.





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$E = 12.5 \text{ GPa}$ $\sigma_{\text{all}} = 12 \text{ MPa}$ $\begin{cases} P = 100 \text{ N} \\ P = 200 \text{ N} \end{cases}$

$L = 2 \text{ m}$

$\rho: P = 100 \times 2.5 = 250 \text{ N}$

مسئله: نیروی درین بار P را ضرب ابعاد 2.5 باشد؟

$P_{\text{cr}} = \frac{\pi^2 EI}{L^2} \rightarrow I = 8.106 \times 10^{-6} \text{ m}^4$ $I = \frac{1}{12} a^4$

$\rightarrow a = 100 \text{ mm}$ $\sigma = \frac{P}{A} = \frac{100}{A} = 10 \text{ MPa} < 12 \text{ MPa}$

$\rho: P = 200 \times 2.5 = 500 \rightarrow I = 16.21 \times 10^{-6} \text{ m}^4 \rightarrow a = 118.1 \text{ mm}$

$\sigma = \frac{P}{A} = 14.34 > 12 \rightarrow$ *سین مقدار ابعاد کوچکتر*

$A = \frac{P}{\sigma_{\text{all}}} = \frac{200}{12 \times 10^6} = 16.67 \times 10^{-3} \text{ m}^2 \rightarrow a = 129.1 \text{ mm} \approx 130 \text{ mm}$

$E = 29 \times 10^6 \text{ psi}$ $\rho: P$ *مسئله: نیروی درین بار P را ضرب ابعاد 3 باشد؟*

$\rho: F_{AB} = \frac{P}{1.06}$

$F_{AB} = \frac{\pi^2 E I_{AB}}{(L_{AB})^2} = \frac{\pi^2 (29 \times 10^6) (\frac{\pi}{4} (\frac{5}{16})^4)}{(1.18^2 + 0.18^2)} = 3308 \text{ lb}$

$L_{AB} = 18^2 + 18^2 = 648$

$F_{AB}/3 = \frac{3308}{3} \rightarrow P = 1.06 \times \frac{3308}{3} = 1169 \text{ lb}$



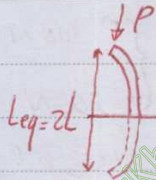
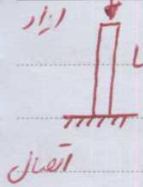
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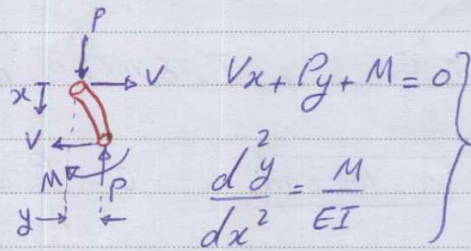
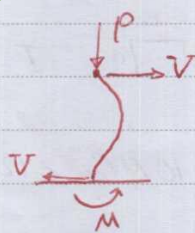
① ثابت



$$P_{cr} = \frac{\pi^2 EI}{L_e^2} = \frac{\pi^2 EI}{4L^2}$$

$$\sigma_{cr} = \frac{\pi^2 E}{\left(\frac{L_e}{r}\right)^2}$$

② ثابت



$$\left. \begin{aligned} Vx + Py + M &= 0 \\ \frac{d^2 y}{dx^2} &= \frac{M}{EI} \end{aligned} \right\}$$

$$\rightarrow \frac{d^2 y}{dx^2} + \frac{Py}{EI} = -\frac{Vx}{EI}$$

$$\alpha^2 = \frac{P}{EI}$$

حل معادله
فرانسوی

$$y = (\text{حل همگن}) + (\text{حل غیر همگن}) \quad y = A \sin \alpha x + B \cos \alpha x + \left(-\frac{Vx}{P}\right)$$

$$\left. \begin{aligned} \text{شرایط مرزی} \\ \left\{ \begin{aligned} x=0 \\ y=0 \end{aligned} \right\} \Rightarrow B=0 \quad \left\{ \begin{aligned} x=L \\ y=0 \end{aligned} \right\} \Rightarrow A \sin \alpha L = \frac{V L}{P} \quad (1) \end{aligned} \right.$$

$$\left\{ \begin{aligned} x=L \\ \frac{dy}{dx}=0 \end{aligned} \right\} \Rightarrow A \alpha \cos \alpha L = \frac{V}{P} \quad (2)$$

$$\tan(\alpha L) = \alpha L \quad \text{از معادله (2) در (1) جایگزین می‌کنیم}$$

$$\alpha^2 = \frac{(4.4934)^2}{L^2}$$

$$\alpha L = 4.4934 \quad \text{از جدول ضرایب}$$

$$\alpha^2 = \frac{P}{EI} \rightarrow P = \frac{20.19 EI}{L^2} = \frac{\pi^2 EI}{(10.7L)^2} \Rightarrow \boxed{L_{eq} = 0.7L}$$

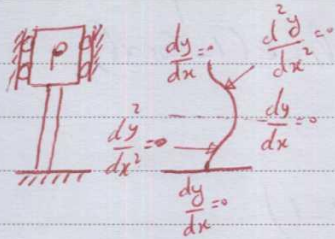


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③ ثابت

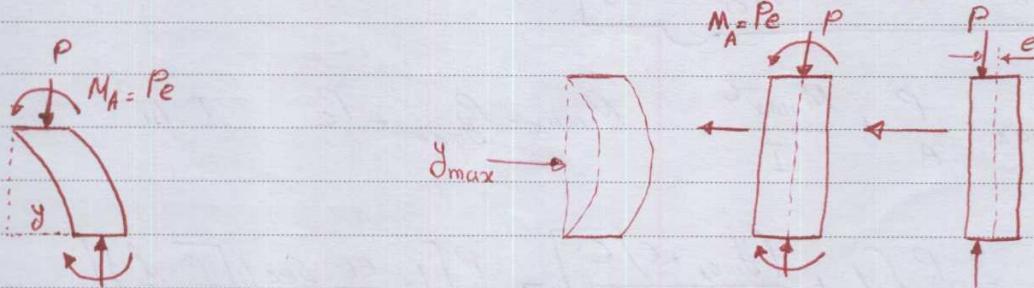


$$L_{eq} = 0.5L \quad P_{cr} = \frac{\pi^2 EI}{(0.5L)^2}$$

تغییر بارها و طول ستون رو بنویسید

	L_{eq}	
دو سر لولا	$1L$	$1 P_{cr}$
دو سر اتصال	$0.5L$	$4 P_{cr}$
یک سر لولا یک سر اتصال	$0.7L$	$2 P_{cr}$
یک سر اتصال یک سر آزاد	$2L$	$0.25 P_{cr}$

با روشی خارج از مرسوم:



$$M + M_A + Py = 0 \rightarrow M = -Py - M_A$$

$$\frac{d^2y}{dx^2} = \frac{M}{EI} = \frac{-Py - M_A}{EI} \rightarrow \frac{d^2y}{dx^2} + \frac{Py}{EI} = -\frac{M_A}{EI} \quad \alpha^2 = \frac{P}{EI}$$

$$\frac{d^2y}{dx^2} + \alpha^2 y = -\alpha^2 e \quad y = A \sin \alpha x + B \cos \alpha x - e$$

$$\begin{cases} x=0 \\ y=0 \end{cases} \Rightarrow B=e$$



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$$= 2 \sin^2 \alpha \frac{l}{2}$$

$$\begin{cases} x=l \\ y=0 \end{cases} \quad A \sin \alpha l + e \cos \alpha l - e = 0 \Rightarrow A \sin \alpha l = e(1 - \cos \alpha l)$$

$$A = e \tan \frac{\alpha l}{2} \quad y = e \left(\tan \frac{\alpha l}{2} \sin \alpha x + \cos \alpha x - 1 \right)$$

$$\rightarrow y_{\max} \xrightarrow{x=\frac{l}{2}} y_{\max} = e \left(\tan \frac{\alpha l}{2} \sin \frac{\alpha l}{2} + \cos \frac{\alpha l}{2} - 1 \right)$$

$$= e \left(\frac{\sin^2 \frac{\alpha l}{2} + \cos^2 \frac{\alpha l}{2}}{\cos \frac{\alpha l}{2}} - 1 \right) = e \left(\sec \frac{\alpha l}{2} - 1 \right)$$

$$y_{\max} = e \left[\sec \left(\sqrt{\frac{P}{EI}} \frac{l}{2} \right) - 1 \right] \rightarrow \sqrt{\frac{P}{EI}} \frac{l}{2} = \frac{\pi}{2} \rightarrow \frac{P}{EI} = \frac{\pi^2 EI}{l^2}$$

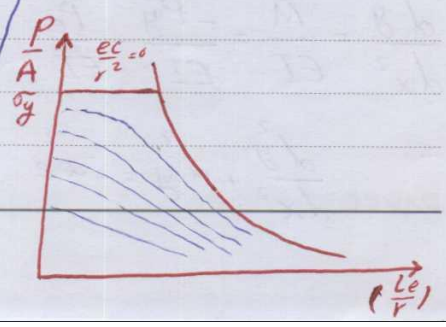
$$y_{\max} = e \left[\sec \left(\frac{\pi}{2} \sqrt{\frac{P}{P_{cr}}} \right) - 1 \right]$$

$$\sigma_{\max} = \frac{P}{A} + \frac{M_{\max} c}{I} \quad M_{\max} = P y_{\max} + P e \quad I = A r^2$$

$$\sigma_{\max} = \frac{P}{A} \left[1 + \frac{(y_{\max} + e) c}{r^2} \right] = \frac{P}{A} \left[1 + \frac{ec}{r^2} \sec \left(\sqrt{\frac{P}{EI}} \frac{l}{2} \right) \right]$$

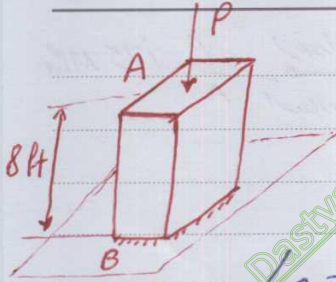
$$\rightarrow \sigma_{\max} = \frac{P}{A} \left[1 + \frac{ec}{r^2} \sec \frac{\pi}{2} \sqrt{\frac{P}{P_{cr}}} \right]$$

$$\frac{P}{A} = \frac{\sigma_{\max}}{1 + \frac{ec}{r^2} \sec \left(\frac{l}{2} \sqrt{\frac{P}{EA}} \frac{l}{r} \right)}$$





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$A = 3.54 \text{ in}^2$ $I = 8 \text{ in}^4$ $r = 1.5 \text{ in}$
 $c = 2 \text{ in}$

افعال برای ضریب ایمنی 2 مقدار بار تنش برابر است با بار اعصاب کنید

$e = 2 \times 8 = 16$ $P_{cr} = \frac{\pi^2 EI}{L_e^2} = 62.1 \text{ kips}$

$P_{all} = \frac{P_{cr}}{F.S} = 31.1 \text{ kips}$ $\sigma_{all} = \frac{P_{all}}{A} = 8.8 \text{ ksi}$

ب. اگر نیروی وارده را اندازیم 0.75 in خارج از مرکز باشد بیشترین مقدار تنش بعد از است این است

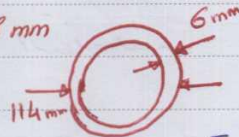
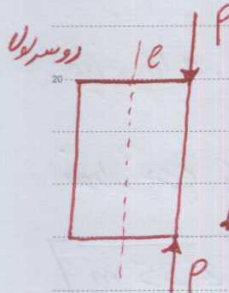
$y_{max} = e \left[\text{Sec} \left(\frac{\pi}{2} \sqrt{\frac{P}{P_{cr}}} \right) - 1 \right] = 0.75 \left[\text{Sec} \left(\frac{\pi}{2} \sqrt{\frac{31.1}{62.1}} \right) - 1 \right]$ max را نیز حساب کنید

$\rightarrow y_{max} = 0.939 \text{ in}$ ← در این نقطه بیشترین

$\sigma_{max} = \frac{P}{A} \left[1 + \frac{ec}{r^2} \text{Sec} \left(\frac{\pi}{2} \sqrt{\frac{P}{P_{cr}}} \right) \right] = \frac{31.1}{3.54} \left[1 + \frac{(0.75)(2)}{(1.5)^2} \text{Sec} \left(\frac{\pi}{2} \right) \right]$

$\rightarrow \sigma_{max} = 22 \text{ ksi}$

مطوب است بارها P اثر: $e = 15.2 \text{ mm}$, $e = 7.6 \text{ mm}$ اگر ضریب ایمنی 2.5 باشد
 $\sigma_y = 250 \text{ MPa}$ $E = 200 \text{ GPa}$



$I = \frac{\pi r^4}{4}$ $L_e = l = 2438 \text{ mm}$

$I = \frac{\pi}{4} \left[(157)^4 - (151)^4 \right] = 30 \times 10^6 \text{ mm}^4$

$A = \frac{\pi}{4} \left[(114)^2 - (102)^2 \right] = 2035 \text{ mm}^2$ $r = \sqrt{\frac{I}{A}} = 38.3 \text{ mm}$



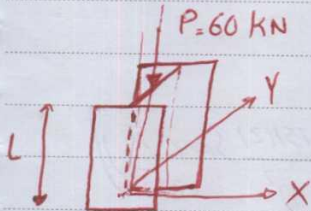
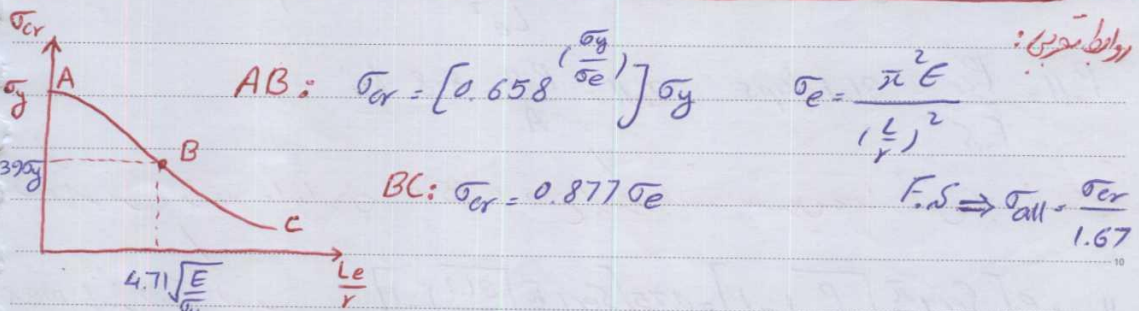
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$$\frac{L_e}{r} = \frac{2438}{38.3} = 63.6 \quad \frac{eC}{r^2} = \frac{17.61(57)}{(38.3)^2} = 0.295 \quad \text{از نمودار استاندارد منحنی A} \quad P = 175 \text{ MPa}$$

$$P = 181125 \text{ N} \rightarrow P_{\text{allow}} = \frac{P}{F.S} = 72450 \text{ نیوتن}$$



S 100 x 11.5 E = 200 GPa $\sigma_y = 250 \text{ MPa}$: منوال

از منحنی روابط تجربی $\sigma_{cr, max}$ استفاده کنید.

$$A = 1460 \text{ mm}^2, \quad r_x = 41.6 \text{ mm}, \quad r_y = 14.8 \text{ mm}$$

$$\sigma_{all} = \frac{P}{A} = \frac{60 \times 10^3}{1460 \times 10^{-4}} = 41.1 \text{ MPa}$$

چون $\sigma_{all} = 0.16 \sigma_y$ بنابراین باید از قسمت BC استفاده کنید.

$$\sigma_{cr} = 0.877 \sigma_e = 0.877 \frac{\pi^2 E}{\left(\frac{L}{r} \right)^2}$$

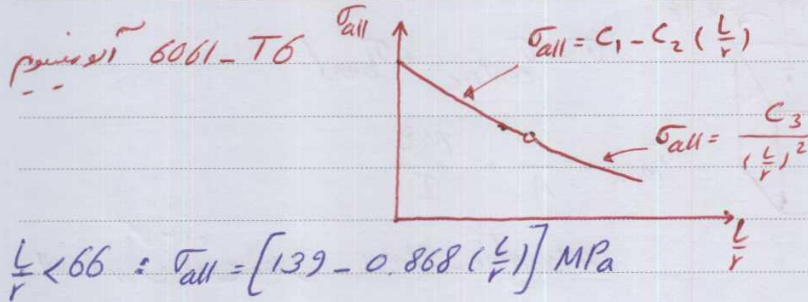
نمودار تجربی AISC استفاده کنید.

$$= \frac{0.877 (\pi^2) (200 \times 10^9)}{\left(\frac{L}{r} \right)^2} = 41.1 \times 10^6 \rightarrow \frac{L}{r} = 158.8 \rightarrow L = 2.35 \text{ m}$$



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روابط تجربی:



$\frac{L}{r} < 66 : \sigma_{all} = [139 - 0.868 \left(\frac{L}{r}\right)] \text{ MPa}$

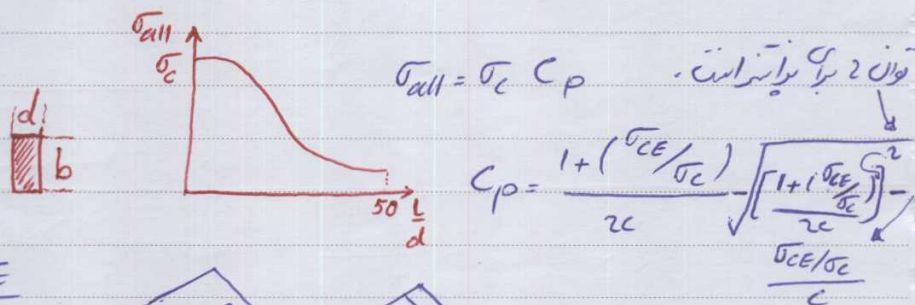
$\frac{L}{r} > 66 : \sigma_{all} = \frac{351 \times 10^3}{\left(\frac{L}{r}\right)^2} \text{ MPa}$

2014-T6 آلومینیوم

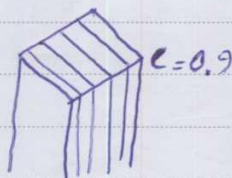
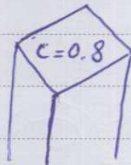
$\frac{L}{r} < 55 : \sigma_{all} = [212 - 1.585 \left(\frac{L}{r}\right)] \text{ MPa}$

$\frac{L}{r} > 55 : \sigma_{all} = \frac{372 \times 10^3}{\left(\frac{L}{r}\right)^2} \text{ MPa}$

wood (چوب)



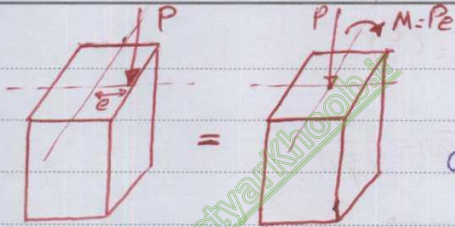
$\sigma_{CE} = \frac{0.822 E}{\left(\frac{L}{d}\right)^2}$





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$$\sigma = \sigma_{\text{centric}} + \sigma_{\text{bend}}$$

$$\sigma_{\text{max}} = \frac{P}{A} + \frac{MC}{I}$$

Allowable-stress الف، روش تنش مجاز



$$\frac{P}{A} + \frac{MC}{I} \leq \sigma_{\text{all}}$$

Interaction Method ب، روش برهم‌کنش

$$\frac{\frac{P}{A}}{(\sigma_{\text{all}})_{\text{axial}}} + \frac{\frac{MC}{I}}{(\sigma_{\text{all}})_{\text{bending}}} \leq 1 \quad \sigma_{\text{all bending}} > \sigma_{\text{all axial}}$$



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